

TITLE OF THE INVENTION

DIGITAL BASEBAND MODULATION APPARATUS AND  
DEMODULATION APPARATUS

5 BACKGROUND OF THE INVENTION

1. Field of the Invention

The present invention relates to digital  
baseband modulation/demodulation apparatuses. More  
particularly, the present invention relates to  
10 digital baseband modulation/demodulation apparatuses  
applicable to base stations or mobile stations in a  
CDMA (Code Division Multiple Access) cellular  
communication system in which spread spectrum  
modulation by QPSK is performed as a primary  
15 modulation method.

In the next generation cellular phone  
system represented by IMT-2000, it is required to  
realize large capacity packet transmission system  
called HSDPA (High Speed Downlink Packet Access). In  
20 addition, it is desired to miniaturize apparatuses  
used in the system and to reduce power consumption  
of the apparatuses.

2. Description of the Related Art

Figs.1A, 1B and Fig.2 are diagrams for  
25 explaining a conventional technology. Fig.1A is a  
block diagram showing a three level QPSK modulation  
apparatus applicable to the IMT-2000 standard. The  
number 11 indicates a spread modulation part for  
complex spreading a pair of an  $I_c$  component and a  $Q_c$   
30 component of an input digital signal by using  
spreading code  $I_s$  and  $Q_s$ , wherein  $I_s$  corresponds to  
the I axis, and  $Q_s$  corresponds to the Q axis. The  
number 12 shows a phase rotation part for rotating  
the phase of the output signal from the spread  
35 modulation part 11. Fig.2 is a block diagram of a  
demodulation apparatus corresponding to the  
modulation apparatus shown in Fig.1A. In Fig.2, 45

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indicates a phase reverse rotation part and 46  
indicates a despread demodulation part.

In Fig.1A, a complex spread output signal  
(I, Q) output from the spread modulation part 11 is  
5 represented as:

$$I = I_c \cdot I_s - Q_c \cdot Q_s$$

$$Q = I_c \cdot Q_s + Q_c \cdot I_s$$

where  $I_c$  is send information spread by  
channelization code  $C_d$ ,  $Q_c$  is source information  
10 spread by channelization code  $C_c$ ,  $I_s$  is spreading  
code for the I axis, and  $Q_s$  is spreading code for  
the Q axis.

The pair of I and Q component signals can  
be represented as complex representation as follows  
15 in which I corresponds to the real number axis and Q  
corresponds to the imaginary number axis:

$$I + jQ = A_c \cdot A_s \cdot e^{j(\phi_c + \phi_s)}$$

where  $A_c$  is the amplitude of a signal  $I_c + jQ_c$ ,  $\phi_c$  is  
the phase of  $I_c + jQ_c$ ,  $A_s$  is the amplitude of the  
20 signal  $I_s + jQ_s$ , and  $\phi_s$  is the phase of  $I_s + jQ_s$ .

The spread modulation part 11 has a  
transmit interrupt function (DXT) formed by AND  
gates A1-A4. The phase rotation part 12 is a part  
of a transmit diversity function for transmitting  
25 the same source information signals by shifting the  
phases.

Fig.1B shows constellations on a complex  
plain for the modulation apparatus. In the figure,  
(a) shows a case where there is no phase rotation,  
30 and the signal amplitude on I/Q axes takes three  
levels (1, 0, -1), and there are five signal points  
including the origin point (I, Q)=(0, 0). In the  
figure, (b) shows a case where there is a phase  
rotation of  $45^\circ$  in which there are 9 signal points.

35 However, if the constellation in which the  
phase is rotated is adopted, the amplitude (2) of a  
signal output only on the I axis or only on the Q

axis by the spread modulation part is two times of  
the amplitude (1) of other signal points. That is,  
2 bits are necessary in a signal amplitude part.  
This results in increasing of the circuit size and  
5 the power consumption of the baseband  
modulation/demodulation apparatus.

#### SUMMARY OF THE INVENTION

An object of the present invention is to  
10 provide digital baseband modulation/demodulation  
apparatuses for realizing high speed transmission  
while decreasing the size and the power consumption  
of the apparatuses.

The above object is achieved by a digital  
15 baseband modulation apparatus, including:

a spread modulation part for complex  
spreading an I component signal and a Q component  
signal of a transmit signal by using spreading code  
for I axis and spreading code for Q axis so as to  
20 output an output signal comprising an output I  
component signal and an output Q component signal;  
and

an amplitude conversion part for  
decreasing the amplitude component of the output  
25 signal to the half when the output signal is output  
on the I axis or on the Q axis.

According to the present invention, the  
size (number of bits and the like) of the process  
circuits and transmit power consumption can be  
30 decreased. Thus, the size of the whole circuits can  
be downsized.

The above object is also achieved by a  
digital baseband demodulation apparatus, including:

a part for quadrature detecting an I  
35 component signal and a Q component signal from a  
received signal;

an amplitude reverse conversion part for

doubling the amplitude component of the received signal when the received signal is on the I axis or on the Q axis; and

5 a despread demodulation part for complex despread the I component signal and the Q component signal by using spreading code for I axis and spreading code for Q axis to obtain a complex despread signal.

10 According to the present invention, the size (number of bits and the like) of the process circuits for air interface and receive power consumption can be decreased. Thus, the size of the whole circuits can be downsized.

15 BRIEF DESCRIPTION OF THE DRAWINGS

Other objects, features and advantages of the present invention will become more apparent from the following detailed description when read in conjunction with the accompanying drawings, in  
20 which:

Fig.1A is a block diagram showing a three level QPSK modulation apparatus applicable to the IMT-2000 standard;

25 Fig.1B shows constellations on a complex plain for the modulation apparatus shown in Fig.1A;

Fig.2 is a block diagram of a demodulation apparatus corresponding to the modulation apparatus shown in Fig.1A;

30 Fig.3A shows a constellation for explaining the principle of the present invention in modulation;

Fig.3A shows a constellation for explaining the principle of the present invention in demodulation;

35 Fig.4 is a block diagram showing a part of a communication apparatus (for example, a mobile terminal) which is based on an embodiment of the

present invention;

Fig.5A is a block diagram of a modulation part which is based on the first embodiment of the present invention;

5 Fig.5B is a block diagram of a demodulation part which is based on the first embodiment of the present invention;

Fig.6A shows constellations before and after performing amplitude conversion process which is based on the first embodiment of the present invention;

Fig.6B is a truth table used for realizing the above-mentioned amplitude conversion process;

15 Fig.6C is a logic circuit diagram for realizing the above-mentioned truth table;

Fig.7A shows constellations before and after performing amplitude reverse conversion process which is based on the first embodiment of the present invention;

20 Fig.7B is a truth table for realizing the above-mentioned amplitude reverse conversion process;

Fig.7C is a logic circuit diagram for realizing the above-mentioned truth table;

25 Fig.8A is a block diagram of a modulation part which is based on the second embodiment of the present invention;

30 Fig.8B shows the constellation of a duplexed signal which is based on the second embodiment of the present invention;

Fig.9 is a diagram for explaining a process for duplexing signal points which is based on the second embodiment;

35 Fig.10A is a block diagram of the demodulation part which is based on the second embodiment of the present invention;

Fig.10B shows reverse conversion

characteristics of the amplitude reverse conversion part which is based on the second embodiment of the present invention;

5 Fig.11 is a block diagram of a modulation part of the third embodiment of the present invention;

Fig.12A is a block diagram of a modulation part which is based on the fourth embodiment of the present invention;

10 Fig.12B shows a constellation after the offset values are added which is based on the fourth embodiment of the present invention.

#### DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

15 First, an outline of embodiments of the present invention is described in the following. A digital baseband modulation apparatus of the present invention includes: a spread modulation part for complex spreading an I component signal and a Q  
20 component signal of a transmit signal by using spreading code for I axis and spreading code for Q axis so as to output an output signal comprising an output I component signal and an output Q component signal; and an amplitude conversion part for  
25 decreasing the amplitude component of the output signal to the half when the output signal is output on the I axis or on the Q axis.

For example, as shown in Fig.3A, the amplitude conversion part converts signals  $(I, Q) = (-2, 0), (2, 0), (0, -2),$  and  $(0, 2)$ , output from the  
30 spread modulation part on the I axis or the Q axis, into  $(I, Q) = (-1, 0), (1, 0), (0, -1),$  and  $(0, 1)$ . That is, the amplitude component (=2) of the output signal is decreased to the half (=1).

35 In the digital baseband modulation apparatus, the spread modulation part may include a phase rotation part for rotating the phase angle of

the output signal according to a control from the outside. Thus, transmit diversity can be efficiently realized by rotating the phase.

A digital baseband demodulation apparatus of the present invention includes: a part for quadrature detecting an I component signal and a Q component signal from a received signal; an amplitude reverse conversion part for doubling the amplitude component of the received signal when the received signal is on the I axis or on the Q axis; and a despread demodulation part for complex despread the I component signal and the Q component signal by using spreading code for I axis and spreading code for Q axis to obtain a complex despread signal.

As shown in Fig.3B, the amplitude reverse conversion part doubles the amplitude component (=1) of the received signal  $(I, Q) = (-1, 0), (1, 0), (0, -1)$  and  $(0, 1)$  that are on the I axis or on the Q axis. Accordingly, the signals  $(I, Q) = (-1, 0), (1, 0), (0, -1)$  and  $(0, 1)$  are reconstructed to  $(I, Q) = (-2, 0), (2, 0), (0, -2)$  and  $(0, 2)$ .

In the digital baseband demodulation apparatus, the despread demodulation part may include a phase rotation part for rotating the phase of the complex despread signal according to a control from the outside. Thus, receive diversity can be efficiently realized by rotating the phase.

In addition, another digital baseband modulation apparatus of the present invention includes, as shown in Fig.8A, a plurality of pairs of the above-mentioned spread modulation part and the above-mentioned amplitude conversion part; a duplexing part for duplexing output signals output from the amplitude conversion parts by linearly adding the output signals; a separation part for separating a received high speed channel signal into

a plurality of separated signals to be input into the spread modulation parts; and a switch part for switching between the separated signals and received low speed channel signals to input the separated  
5 signals or the received low speed channel signals into the spread modulation parts.

Fig.8B shows a constellation of the signal output from the duplexing part 16. Since each amplitude component of signals output from the  
10 amplitude conversion parts on the I axis or on the Q axis are decreased to the half, the amplitude component of the duplexed signal is also decreased. Thus, the large capacity data transmission (HSDPA) can be realized with smaller circuit and lower power  
15 consumption. In the digital baseband modulation apparatus, the duplexing part may add an offset value to each I component signal when the value of the I component signal is 0 and add an offset value to each Q component signal when the value of the Q  
20 component signal is 0. By adding the offset value to prevent I component or Q component from becoming 0. Accordingly, the process amount of a signal processing part can be decreased and dynamic range of a power amplifying part can be decreased.

25 In the following, embodiments of the present invention will be described. Same symbols are assigned to the same or corresponding parts throughout the drawings.

Fig.4 is a block diagram showing a part of  
30 a communication apparatus (for example, a mobile terminal) which is based on an embodiment of the present invention. In the figure, 11 is a spread modulation part, 12 is a phase rotation part, 13 is an amplitude conversion part, 31 is a D/A conversion  
35 part, 32 is a quadrature modulation part (QMOD), 33 is a RF modulation part (TX) for up converting the quadrature modulated signal to the RF signal, 34 is



a transmit/receive wave switch part, 35 is an antenna, 41 is a RF demodulation part (RX) for down converting the received RF signal to the baseband signal, 42 is a quadrature demodulation part (QDEM), 43 is an A/D conversion part, 44 is an amplitude reverse conversion part, 45 is a phase rotation part, 46 is a despread demodulation part, 47 is a detector part, 48a and 48b show each finger part, 49 is a path combination part (RAKE combination part), and 50 is a searcher.

Figs.5A and 5B are block diagrams of the modulation/demodulation parts which are based on the first embodiment, in which a pair of the I component channel signal and the Q component signal is modulated/demodulated. Fig.5A is a block diagram of the modulation part. The modulation part includes the spread modulation part 11, the phase rotation part 12 and the amplitude conversion part 13 in which the amplitude conversion part 13 is provided at the back of the phase rotation part 12. Fig.5B is a block diagram of the demodulation part that includes the amplitude reverse conversion part 44, the phase reverse rotation part 45 and the despread demodulation part 46 in which the phase reverse rotation part 45 and the despread demodulation part 46 are provided behind the amplitude reverse conversion part 44.

Figs.6A-6C are diagrams for explaining the amplitude conversion part according to the first embodiment. Fig.6A shows constellations before and after performing the amplitude conversion process. The amplitude of the input signal on the I or Q axis takes one of three levels of (-2, 0, 2). The amplitude of other signals takes one of three levels of (-1, 0, 1). The amplitude conversion part reduces the amplitude (=2) of the signal on the I axis or the Q axis into the half. That is, the

signals  $(I, Q) = (-2, 0), (2, 0), (0, -2)$  and  $(0, 2)$  are converted to signals  $(I, Q) = (-1, 0), (1, 0), (0, -1)$  and  $(0, 1)$  respectively. Therefore, the size (number of bits and the like) of the process circuits and transmit power consumption can be decreased.

Fig.6B is a truth table used for the above-mentioned amplitude conversion process. As shown in the table, only when the amplitude component  $(I1, I0)$  or  $(Q1, Q0)$  of the input signal is  $(1, 0)$  or  $(0, 1)$ , the amplitude component  $(I0)$  or  $(Q0)$  is converted to 1 and only the one bit is output. Accordingly, the amplitude component of the output signal can be reduced to 1 bit.

Fig.6C is a logic circuit diagram that realizes the above truth table. As shown in the figure, the 1 bit sign of the input signal  $SI/SQ$  is output as it is. As to two bits amplitude components  $(I1, I0)$  and  $(Q1, Q0)$ , EX-OR is calculated between  $I1$  and  $I0$ , and between  $Q1$  and  $Q0$ , so that amplitude of the output signal can be reduced to 1 bit amplitude component  $I0$  and  $Q0$ .

Figs.7A-7C are diagrams for explaining the amplitude reverse conversion part which are based on the first embodiment. Fig.7A shows constellations before and after performing amplitude reverse conversion process. The amplitude of the input signal of the amplitude reverse part takes one of three levels of  $(-1, 0, 1)$  regardless whether the input signal is on the I/Q axis or not. The amplitude reverse conversion part increases the amplitude ( $=1$ ) of the signal on the I axis or on the Q axis to double ( $=2$ ). That is, signals  $(I, Q) = (-1, 0), (1, 0), (0, -1)$  and  $(0, 1)$  are reconstructed to signals  $(I, Q) = (-2, 0), (2, 0), (0, -2)$  and  $(0, 2)$  respectively. Therefore, the receiving side can be in harmony with the sending side.

Fig.7B is a truth table for realizing the above-mentioned amplitude reverse conversion process. As shown in the table, if  $(I_0, Q_0)$  is  $(1, 0)$  or  $(0, 1)$ , amplitude component  $(I_1, I_0)$ ,  $(Q_1, Q_0)$  is converted to  $(1, 0)$ ,  $(0, 0)$  or  $(0, 0)$ ,  $(1, 0)$  respectively. Accordingly, the amplitude component of each of the I component signal and Q component signal can be reconstructed to two bits, that is,  $(I_1, I_0)$  or  $(Q_1, Q_0)$ .

Fig.7C is a logic circuit diagram for realizing the above truth table. As shown in the figure, 1 bit sign of input signal  $SI/SQ$  is output as it is. As to one bit amplitude component  $(I_0)$  or  $(Q_0)$ , a logic shown in the figure is applied so that two bit amplitude component  $(I_1, I_0)$  or  $(Q_1, Q_0)$  can be reconstructed.

Fig.8A is a block diagram of the modulation part which is based on the second embodiment of the present invention, in which signals of a plurality of channels each comprising a pair of I component signal and Q component signal are duplexed and transmitted. In the figure,  $11_1 - 11_n$  are spread modulation parts,  $13_1 - 13_n$  are amplitude conversion parts,  $14_1 - 14_n$  are switches, 15 is a serial to parallel conversion part (S/P) for separating an input signal of a high speed channel HSCH into signals of low speed channels, and 16 is a duplexing part for linearly adding (duplexing) output signals from the amplitude conversion parts  $13_1 - 13_n$ .

The modulation part accommodates  $n$  low speed channels  $CH_1 - CH_n$  for transmitting sounds and the like, and one high-speed channel HSCH for transmitting image data and the like. Each channel signal includes quadrature pair of the I component signal and the Q component signal.

When each of the switches  $14_1 - 14_n$  is

connected to a terminal a, the  $n$  low speed channel signals are duplexed and sent. When each of the switches  $14_1 - 14_n$  is connected to a terminal b, data of low speed channel signals that are obtained by  
5 separating the high speed channel signal HSCH are duplexed and sent. Fig.8B shows the constellation of the multiplexed signal.

Fig.9 is a diagram for explaining a process for multiplexing signal points which is  
10 based on the second embodiment. For the sake of simplicity, Fig.9 shows a case in which I, Q data of two channels CH1 and CH2 are duplexed (linearly added).

First, signals duplexed on the I or Q axis  
15 will be described. When source data of CH1 is  $(I, Q)=(0, 0)$ , and source data of CH2 is  $(I, Q)=(0, 0)$ , duplexed source data is  $(I, Q)=(0, 0)$ . Next, when source data of CH1 is  $(I, Q)=(0, 0)$ , and source data of CH2 is  $(I, Q)=(0, 1)$ , duplexed source data is  $(I, Q)=(0, 1)$ .  
20 In addition, when source data of CH1 is  $(I, Q)=(0, 1)$ , and source data of CH2 is  $(I, Q)=(0, 0)$ , duplexed source data is also  $(I, Q)=(0, 1)$ . Thus, since both amplitudes are 1, they cannot be distinguished from each other from the viewpoint of  
25 amplitude. However, the former duplexed source data  $(I, Q)=(0, 1)$  are spread/despread by spreading code of CH2, and latter duplexed source data  $(I, Q)=(0, 1)$  are spread/despread by spreading code of CH1. Therefore, they can be distinguished from each other.

30 When source data of CH1 is  $(I, Q)=(0, 1)$ , and source data of CH2 is  $(I, Q)=(0, 1)$ , duplexed source data is  $(I, Q)=(0, 2)$ . The other combinations can be obtained in the same way.

Next, signals duplexed in quadrants other  
35 than the I axis or the Q axis are explained. When source data of CH1 is  $(I, Q)=(0, 0)$ , and source data of CH2 is  $(I, Q)=(1, 1)$ , duplexed source data is  $(I,$

$Q)=(1, 1)$ . In addition, when source data of CH1 is  $(I, Q)=(1, 1)$ , and source data of CH2 is  $(I, Q)=(0, 0)$ , duplexed source data is also  $(I, Q)=(1, 1)$ . When source data of CH1 is  $(I, Q)=(1, 1)$ , and source data of CH2 is  $(I, Q)=(1, 1)$ , duplexed source data is  $(I, Q)=(2, 2)$ .

When both of phase rotation amounts of CH1 and CH2 are equally  $0^\circ$  or  $45^\circ$  (in phase synchronization), there is no combination other than the above-mentioned examples. However, when the phase rotation amounts of CH1 and CH2 are not the same (asynchronous), there are following combinations further. When source data of CH1 is  $(I, Q)=(0, 1)$  (this means that the data reside on the Q axis), and source data of CH2 is  $(I, Q)=(1, 1)$  (this means that the data reside in the first quadrant), duplexed source data is  $(I, Q)=(1, 2)$ . When source data of CH1 is  $(I, Q)=(1, 1)$ , and source data of CH2 is  $(I, Q)=(0, 1)$ , duplexed source data is also  $(I, Q)=(1, 2)$ . Other combinations can be obtained in the same way. As mentioned above, according to the present invention, large amount of information can be transmitted efficiently by utilizing the finite complex I, Q plane (wireless space).

Fig.10A is a block diagram of the demodulation part which is based on the second embodiment of the present invention, in which the demodulation part separates the duplexed received signal into a plurality of signals and demodulates each signal. In the figure, 61 is an amplitude reverse conversion part for reverse converting the amplitude of the duplexed signal, 62 is a hybrid for distributing signals after the amplitude reverse conversion,  $46_1 - 46_n$  are despread demodulation parts corresponding to each separated channel signal,  $63_1 - 63_n$  are switches, and 64 is a parallel to serial conversion part (P/S).

Fig.10B shows reverse conversion characteristics of the amplitude reverse conversion part. As shown in the figure, the input signal ( $\pm N$ , 0) that exists only on I axis is reverse converted to ( $\pm 2N$ , 0) and the input signal (0,  $\pm N$ ) that exists only on Q axis is reverse converted to (0,  $\pm 2N$ ), where N indicates the number of multiplexed channels.

Fig.11 is a block diagram of a modulation part of the third embodiment, in which the modulation part has a transmit diversity function. In the figure,  $12_1 - 12_n$  are phase rotation parts, 17 is a phase control part. In the third embodiment, phase rotation parts  $12_1 - 12_n$  are provided for each channel, so that transmit diversity control can be performed. Thus, communication quality can be improved.

Fig.12A is a block diagram of a modulation part according to the fourth embodiment, in which a predetermined level offset is added to the output signal from the duplexing part. Following offset process is performed in the duplexing part 16. Predetermined offset values  $\Delta I$  and  $\Delta Q$  are added to I and Q levels respectively if the added result becomes a plus level (0 is considered to be +0). Other I and Q component signals are output as it is.

Fig.12B shows a constellation after the offset levels are added. For example, if the duplexed output is (I, Q)=(0, 1), offset values are added such that  $(0+\Delta I, 1+\Delta Q)$ . If (I, Q)=(0, -1), the offset value is added only for the I value such that  $(0+\Delta I, -1)$ . If (I, Q)=(-1, -1), no offset value is added, and the signal is output as it is. Accordingly, since the duplexed output does not include a signal component of level "0", dynamic range of the multiplexed signal can be decreased.

Although the plus I component signal and

the plus Q component signal are shifted to a plus direction in the above-mentioned example, a minus signal component may be shifted to a minus direction. In addition, instead of always adding the offset values, the offset values can be added only when the level of the I component signal or the Q component signal is detected to be "0". In this case, whether the offset is added or not is sent to the receiving side.

10                Although embodiments are described in which the spread modulation parts 11 are provided for each channel, the present invention is not limited to this. The adder used for complex spread modulation can be removed from each spread modulation part 11, and add functions of the removed adders can be centered to an adder of the multiplexing part. Accordingly, the circuit size of the spread modulation parts can be decreased.

20                As mentioned above, according to the present invention, since the size and the power consumption of the digital baseband modulation/demodulation apparatuses can be decreased, large capacity information can be transmitted efficiently at high speed. Thus, the present invention contributes to develop and popularize the next generation cellular phone system and the like.

25                The present invention is not limited to the specifically disclosed embodiments, and variations and modifications may be made without departing from the scope of the present invention

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